

NOTES

A Temperature-Programmed Reaction Method for Catalyst Testing in the Partial Oxidation of Methane to Formaldehyde

During the last years a large variety of unpromoted and promoted oxide catalysts has been claimed to be effective in the partial oxidation of methane (MPO) to formaldehyde (1, 2). This reaction proceeds via a very complex network (2, 3) and requires medium-high temperatures ($550 < T_R < 650^\circ\text{C}$) to attain detectable rates (2). The unique features of the SiO_2 surface in catalysing the formation of partial oxidation products have been largely documented (4–7), while the roles played by MoO_3 , V_2O_5 , Nb_2O_5 , WO_3 , Cr_2O_3 , and other oxides on the reactivity of the SiO_2 (1, 2, 8–13) and the nature of the active centers (1, 2, 6, 9, 11–13) are still topics of debate. A number of papers have particularly addressed the importance of the reaction system (1, 2, 6, 14) and the contribution of the gas phase and/or wall reaction (2, 10, 12, 15) in getting valid and comparable reactivity data. Indeed, since the constraints of the conversion-selectivity relationship (1, 8), suitable reactor device must exploit a differential methane conversion level per pass as to ensure high selectivity to HCHO providing also finite conversion values for a reliable kinetic analysis of the data (6, 12, 14).

In this note we present the potentiality of the temperature-programmed reaction (TPR) method (16) in evaluating the activity of the MPO catalysts. A preliminary comparative analysis of the catalytic performances of bare SiO_2 and various silica supported oxide (MoO_3 , V_2O_5 , Nb_2O_5) catalysts is reported.

4 wt% $\text{MoO}_3/\text{SiO}_2$, 5 wt% $\text{V}_2\text{O}_5/\text{SiO}_2$, and 2 wt% $\text{Nb}_2\text{O}_5/\text{SiO}_2$ catalysts were prepared by incipient wetness impregnation of a pre-

cipitated SiO_2 support (Grade Si 4-5P, Akzo Product; BET S.A., $395 \text{ m}^2 \cdot \text{g}^{-1}$) (12). Ammonium heptamolybdate and ammonium metavanadate in ammonia solution ($\text{pH} \approx 11$) and niobium chloride in HCl solution ($\text{pH} \approx 1$) were used as oxide precursors. After impregnation, all the catalysts were dried at 90°C for 24 h and then calcined in air atmosphere at 600°C for 16 h.

TPR measurements were performed in a conventional flow apparatus by using a linear quartz microreactor (i.d., 4 mm; length, 200 mm) connected *on line* with a Thermo-lab (Fisons Instruments) Quadrupole Mass Spectrometer for continuous analysis of the reaction mixture (transit time < 0.5 s). The tests were run in the T range 200 – 650°C by adopting a heating rate (β) of $15^\circ\text{C} \cdot \text{min}^{-1}$ and a $\text{He}/\text{CH}_4/\text{O}_2$ reaction mixture in the molar ratio 7/2/1 flowing at $50 \text{ STPml} \cdot \text{min}^{-1}$ over 0.05 g of catalyst (F/W , $16.7 \text{ ml} \cdot \text{s}^{-1} \cdot \text{g}^{-1}$). Before the tests, catalyst samples were further conditioned *in situ* at 600°C for 1 h under a 15% O_2/He flow. Mass spectra were recorded in multiple ion monitoring (MIM) mode using the SEM amplifier operating at 1200 V (total pressure, 2×10^{-9} bar) and an ionization potential of -70 V. TPR spectra have been obtained by acquiring the signals relative to the following m/z values: 2 (H_2), 4 (He), 15 (CH_3), 17 (OH), 28 (CO), 29 (CHO), 30 (HCHO), 32 (O_2), and 44 (CO_2). Then, CH_4 consumption has been detected by CH_3 signal, while HCHO formation has been revealed by following CHO and HCHO masses. By using He as internal standard, CH_4 and O_2 conversion values were derived from the CH_3/He and O_2/He signal ratios, respectively. For the calcula-

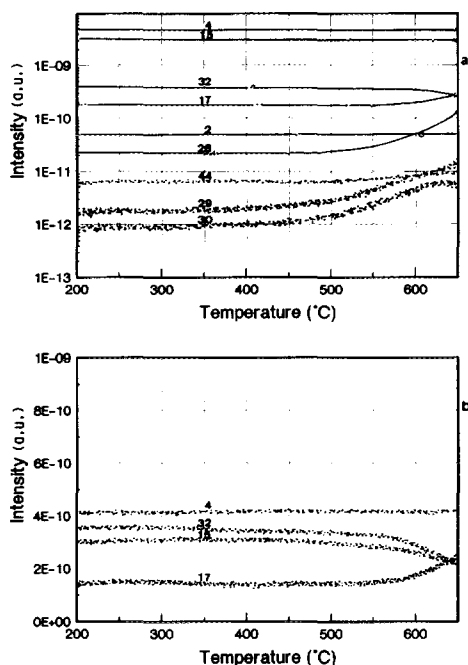


FIG. 1. Partial oxidation of methane over the 5% V_2O_5/SiO_2 catalyst. (a) TPR profiles of: $m/z = 2$, H_2 ; $m/z = 4$, He; $m/z = 15$, $CH_3(CH_4)$; $m/z = 17$, OH; $m/z = 28$, CO; $m/z = 29$, CHO; $m/z = 30$, HCHO; $m/z = 32$, O_2 ; $m/z = 44$, CO_2 . (b) TPR profiles of He (m/z , 4), CH_4 (m/z , 15), O_2 (m/z , 32) and H_2O (m/z , 17) in a linear scale. ($m/z = 4$ and $m/z = 15$ have been multiplied by a factor of 0.1). Experimental conditions: β , $15^\circ C \cdot min^{-1}$; W_{cat} , 0.05 g; reaction mixture flow, $50 ml \cdot min^{-1}$ (He/ $CH_4/O_2 = 7/2/1$).

tion of the relative abundance of HCHO, CO and CO_2 species the integral factors 0.93, 0.468, and 0.78 for m/z 28 (CO), 29 (CHO), and 44 (CO_2), respectively, have been used (17). The carbon mass-balance, estimated by the cross-check of the CH_4 conversion values calculated on the basis of the products formed with those obtained from the CH_3/He signal ratio, resulted within $\pm 7\%$.

The complete TPR spectrum of the 5% V_2O_5/SiO_2 catalyst is shown in Fig. 1a. Further, in a linear scale the traces of He (m/z , 4), CH_4 (m/z , 15), O_2 (m/z , 32), and H_2O (m/z , 17) are displayed in Fig. 1b. It can be noted that the background partial pressure of the selected masses (m/z) keeps unchanged up to the temperature (T_0) at which

the 5% V_2O_5/SiO_2 system begins to explicate its catalytic action which results in the formation of HCHO, CO, CO_2 and H_2O . Afterwards, a monotonically increase in the rate of product formation (Fig. 1a) and a concomitant decrease in the intensity of the signals related to CH_3 and O_2 species (Fig. 1b) have been observed. Such a trend has been experienced for all the investigated systems. However, in Fig. 2 a direct proof of the reactivity of unpromoted SiO_2 (Fig. 2a), 4% MoO_3/SiO_2 (Fig. 2b), 5% V_2O_5/SiO_2 (Fig. 2c), and 2% Nb_2O_5/SiO_2 (Fig. 2d) catalysts arises from the patterns related to the signals of CO, HCHO and CO_2 . These patterns provide peculiar catalytic features allowing to establish both the onset temperature (T_0) at which the formation of each reaction product begins and the extent of product formed.

For the sake of comparison, the T_0 's values for the different catalytic systems are listed in Table 1. Some important points emerge from these data:

(i) on the 5% V_2O_5/SiO_2 catalyst formaldehyde is detected at a T ($T_{o,HCHO} = 460^\circ C$) lower than that found ($T_{o,HCHO} = 500^\circ C$) for the bare silica, by contrast, $T_{o,HCHO}$ is markedly shifted to higher values on 4% MoO_3/SiO_2 ($T_{o,HCHO} = 580^\circ C$) and 2% Nb_2O_5/SiO_2 ($T_{o,HCHO} = 560^\circ C$) systems;

(ii) both $T_{o,CO}$ and T_{o,CO_2} values for the different systems are in the same sequence observed for $T_{o,HCHO}$;

(iii) the sequence of onset temperature of product formation for all the catalysts is

$$T_{o,HCHO} < T_{o,CO} < T_{o,CO_2}.$$

Points (i) and (ii) allow us to state that the reactivity of the SiO_2 is negatively affected by the addition of MoO_3 and Nb_2O_5 , while V_2O_5 promotes the functionality of the SiO_2 surface towards the formation of partial oxidation products (HCHO, CO) (12). On the other hand, the sequence of onset temperatures provide some elements for envisioning the reaction pathway. Indeed, such sequence undoubtedly signals that the cata-

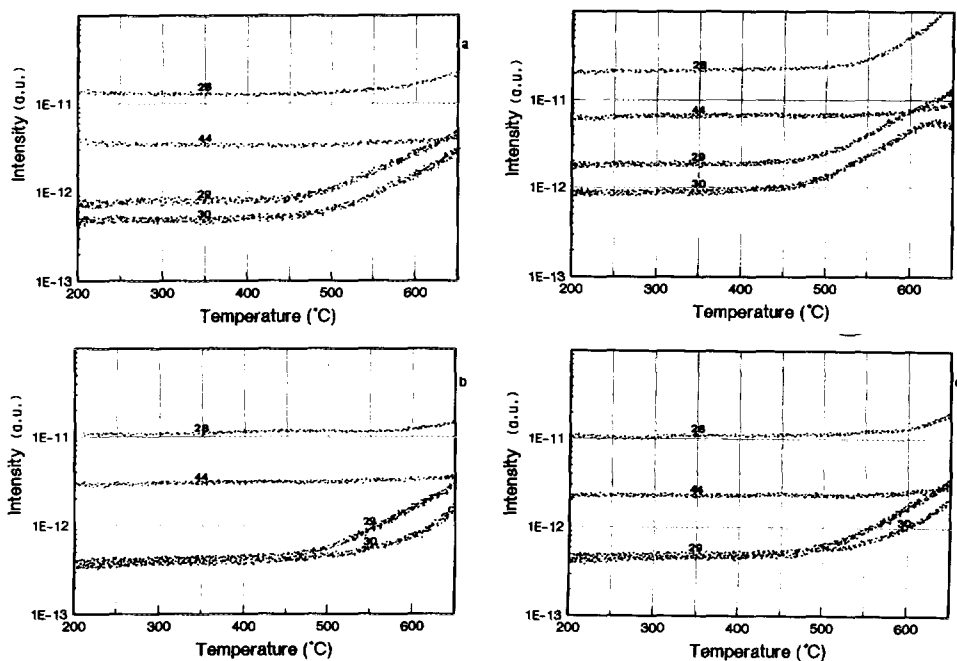
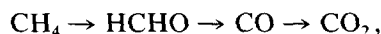


FIG. 2. Partial oxidation of methane over: (a) SiO_2 ; (b) 4% $\text{MoO}_3/\text{SiO}_2$; (c) 5% $\text{V}_2\text{O}_5/\text{SiO}_2$; and (d) 2% $\text{Nb}_2\text{O}_5/\text{SiO}_2$ catalysts. TPR profiles of HCHO ($m/z = 29$ and 30), CO ($m/z = 28$) and CO_2 ($m/z = 44$). Experimental conditions: see Fig. 1.

lytic action of MPO catalysts implies the primary formation of HCHO (1, 2, 9, 18). The formation of CO at T ($T_{o,\text{CO}}$) slightly higher than $T_{o,\text{HCHO}}$ (see Table 1) indicates that CO mainly arises from consecutive reactions (i.e., decomposition and/or oxidation) of formaldehyde on the catalyst surface (3, 9, 18). Moreover, the detection of carbon dioxide at T substantially higher (T_{o,CO_2}) than those found for either HCHO

or CO production could be taken as a probatory evidence of the occurrence of a sequential reaction path (2, 9, 18),



even if at higher reaction temperatures ($>600^\circ\text{C}$) the contribution of a parallel reaction leading directly to CO_2 cannot be completely excluded. Such a hypothesis is sustained by the reaction pattern of the 4% $\text{MoO}_3/\text{SiO}_2$ catalyst. Indeed, the smaller difference between $T_{o,\text{HCHO}}$ and T_{o,CO_2} observed for this system probably reflects the occurrence of a parallel reaction accounting for the formation of carbon dioxide (19).

Further insight into the catalytic behaviour of the studied systems has been gained by a quantitative evaluation of the product amounts (A_{HCHO} , A_{CO} , and A_{o,CO_2}) formed between T_o and 650°C . Such integral area values (A), accounting for the capability of the studied systems in promoting the formation of the different products, have been

TABLE I

Partial Oxidation of Methane on Silica-Supported Oxide Catalysts. Onset Temperature (T_o) of Product Formation

Catalyst	$T_{o,\text{HCHO}}$ ($^\circ\text{C}$)	$T_{o,\text{CO}}$ ($^\circ\text{C}$)	T_{o,CO_2} ($^\circ\text{C}$)
SiO_2	500	540	630
4% $\text{MoO}_3/\text{SiO}_2$	580	600	620
5% $\text{V}_2\text{O}_5/\text{SiO}_2$	460	500	580
2% $\text{Nb}_2\text{O}_5/\text{SiO}_2$	560	610	>650

TABLE 2

Partial Oxidation of Methane on Silica-Supported Oxide Catalysts. Product Amount (A_X) and Product Selectivity (S_X^* , %)

Catalyst	A_{HCHO} (a.u.)	A_{CO} (a.u.)	A_{CO_2} (a.u.)	A_{tot}^a (a.u.)	$S_{\text{HCHO}}^*{}^b$ (%)	$S_{\text{CO}}^*{}^b$ (%)	$S_{\text{CO}_2}^*{}^b$ (%)
SiO_2	5.1	6.5	0.2	11.8	42.8	56.0	1.1
4% $\text{MoO}_3/\text{SiO}_2$	2.2	1.8	0.5	4.5	50.3	42.3	7.4
5% $\text{V}_2\text{O}_5/\text{SiO}_2$	20.1	68.9	5.0	94.0	21.2	75.4	3.4
2% $\text{Nb}_2\text{O}_5/\text{SiO}_2$	3.5	2.8	0.	6.3	54.6	45.4	0.0

$$^a A_{\text{tot}} = A_{\text{HCHO}} + A_{\text{CO}} + A_{\text{CO}_2}$$

$$^b S_X^* = A_X/A_{\text{tot}}$$

summarized in Table 2. Notably, the values we found for the bare SiO_2 , 4% $\text{MoO}_3/\text{SiO}_2$ and 5% $\text{V}_2\text{O}_5/\text{SiO}_2$ fully confirm the reactivity scale previously found under analogous reaction conditions by batch, flow and pulse reactors (12). In particular, the integrated area values of HCHO (A_{HCHO}), which can be taken as a measure of the catalyst capability in driving the MPO (6–12), reveal the strong promoting role of vanadia (A_{HCHO} , 20.1) on the reactivity of silica (A_{HCHO} , 5.1) along with a marked negative effect of molybdenum oxide (A_{HCHO} , 2.2) which likely depresses the peculiar catalytic functionality of the SiO_2 surface (12). Moreover, though oxide loading effects could be invoked (1, 11), the addition of niobium oxide (2 wt%) also yields a lowering in the activity of the SiO_2 support (Table 2). Hence, the values of the total product amount (A_{tot}) listed in Table 2, accounting for the

overall catalytic activity of those systems ($A_{\text{tot}} = A_{\text{HCHO}} + A_{\text{CO}} + A_{\text{CO}_2}$), well highlight the superior performance of the 5% vanadia-promoted silica catalyst (12) with respect either to the unpromoted SiO_2 or 4% $\text{MoO}_3/\text{SiO}_2$ and 2% $\text{Nb}_2\text{O}_5/\text{SiO}_2$ catalysts. In addition, taking into account the bare SiO_2 as reference system, it arises that the highest reactivity of the 5% $\text{V}_2\text{O}_5/\text{SiO}_2$ sample entails a lower integrated selectivity (S_X^*) to formaldehyde (S_{HCHO}^*) with a parallel increase in the selectivity to CO (S_{CO}^*). The opposite pattern, coming down from the constraints imposed by the conversion-selectivity relationship (1, 8), can be observed for both 4% $\text{MoO}_3/\text{SiO}_2$ and 2% $\text{Nb}_2\text{O}_5/\text{SiO}_2$ catalysts. In fact, the higher selectivity to formaldehyde of these systems mostly arises from their worse capability in catalysing the title reaction. Finally, quantitative estimates of CH_4 and O_2 conversion

TABLE 3

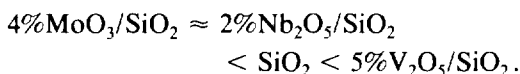
Comparison of Activity Data for Silica and 5% $\text{V}_2\text{O}_5/\text{SiO}_2$ Catalysts Obtained by TPR and Batch Reactor Tests

Catalyst	CH_4 conv. (%)		O_2 conv. (%)		HCHO Sel. (%)		Y_{HCHO}^a		$Y_{\text{HCHO}}^{a,b}$	
	600°C	650°C	600°C	650°C	600°C	650°C	600°C	650°C	600°C	650°C
SiO_2	2.2	4.0	6.9	11.1	49	38	155	224	116	304
5% $\text{V}_2\text{O}_5/\text{SiO}_2$	4.4	13.1	9.9	36.7	31	20	201	386	318	793

^a Productivity of HCHO: $Y_{\text{HCHO}} \cdot g_{\text{HCHO}} \cdot \text{kg}_{\text{cat}}^{-1} \cdot \text{h}^{-1}$.

^b Batch reactor; data from Ref. (12).

(%) and HCHO selectivity (%) at 600 and 650°C for SiO₂ and 5% V₂O₅/SiO₂ catalysts are reported in Table 3. The formaldehyde productivity values (Y_{HCHO} , $g_{\text{HCHO}} \cdot \text{kg}_{\text{cat}}^{-1} \text{h}^{-1}$), calculated from the above TPR conversion and selectivity data, are also compared in Table 3 with the formaldehyde productivity values previously obtained by batch reactor tests (12). The satisfactory agreement emerging between these two sets of data, further proving the positive role of vanadia on the reactivity of the silica in the MPO (12), undoubtedly confirms the validity of this TPR approach. On this account, the following order of reactivity can be drawn:



Notwithstanding the slight difference in the Y_{HCHO} data obtained with TPR and batch reactor tests at 650°C, likely connected with some thermal effects in such nonsteady-state measurements and of the semiquantitative character of the QMS response, the proposed TPR method appears as a powerful tool for both investigating the reactivity of solid catalysts and accelerating the work of catalyst testing in the MPO.

In particular, the onset temperature of product formation (T_0) along with the product amount formed between T_0 and 650°C are suitable and reliable parameters for comparing the activity of the different MPO catalysts.

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